



LAWRENCE
LIVERMORE
NATIONAL
LABORATORY

Prospects for high-gain, high yield NIF targets driven by 2w (green) light

L. J. Suter, S. Glenzer, S. Haan, B. Hammel, K. Manes, N. Meezan, J. Moody, M. Spaeth, L. Divol, K. Oades, M. Stevenson

December 18, 2003

Inertial Fusion Sciences & Applications 2003
Monterey, CA, United States
September 7, 2003 through September 12, 2003

Disclaimer

This document was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor the University of California nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or the University of California. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or the University of California, and shall not be used for advertising or product endorsement purposes.

Prospects for high-gain, high-yield NIF targets driven by 2ω (green) light

L.J. Suter, S. Glenzer, S. Haan, B. Hammel, K. Manes, N. Meezan, J. Moody, M. Spaeth, L. Divol
Lawrence Livermore National Laboratory, University of California, Livermore, CA 94551
K. Oades, M. Stevenson Atomic Weapons Establishment, Aldermaston, UK

The National Ignition Facility (NIF), operating at green (2ω) light, has the potential to drive ignition targets with significantly more energy than the 1.8 MJ it will produce in its baseline, blue (3ω) operations. This results in a greatly increased "target design space", providing a number of exciting opportunities for fusion research including the possibility of ignition experiments with capsules absorbing energies in the vicinity of 1 MJ. We report the progress made exploring 2ω for NIF ignition, including potential 2ω laser performance, 2ω ignition target designs and 2ω Laser Plasma Interaction (LPI) studies.

I. Introduction

For several years we have been exploring the possibility of using green (2ω) light for indirect drive ignition on the National Ignition Facility (NIF). The rationale for this work is the promise of extracting significantly more energy ($\sim 2X$) from NIF green light, as compared to blue (3ω) light, and driving far more energetic capsules than we originally envisioned when we started planning NIF in the early 1990's. This paper attempts to provide a comprehensive picture of the progress we have made exploring 2ω for NIF ignition. First we describe the potential operating regime for NIF at 2ω and how that can translate into a very large "design space" for exploring ignition target designs. We then present the results of 2ω ignition target design studies indicating that we can achieve adequate drive and symmetry with 2ω and show how we might capitalize on the large amount of energy available by electing to trade off coupling efficiency for, say, better symmetry or plasma conditions. These simulations also define plasma conditions for ignition-relevant 2ω Laser-Plasma Interaction (LPI) experiments that have been recently performed. We summarize the results of these experiments using modern beam smoothing techniques which indicate that 2ω LPI is not fundamentally different from 3ω 's. Finally, we show how recent experimental findings on mitigating 2ω laser plasma interaction through reduced intensity and/or judicious choice of plasma composition can be incorporated into ignition target designs.

II. Potential target design space with 2ω

The fundamental requirements of the National Ignition Facility Laser now being constructed at Lawrence Livermore National Laboratory include that it shall be capable of irradiating a

target with 1.8 MJ of $0.35\ \mu\text{m}$ (3ω or "blue") light in an ignition pulse shape peaking at 500 TW.

The 3ω light is produced by a neodymium phosphate glass laser system [1] which first produces infrared or " 1ω " light of $1.053\ \mu\text{m}$ wavelength which is then converted to 3ω light by a pair of KDP crystals [2]. The crystals combine three 1ω photons into one 3ω photon. Ignition pulse shapes require peak power after a long, low power "foot" lasting many nanoseconds. Moreover, this peak power must be produced after a significant amount of energy has already been extracted from the $1\ \mu\text{m}$ laser since crystal tuned to provide optimum, $\sim 70\%$ conversion of 1ω to 3ω at peak power have relatively low conversion during the foot. Since the average conversion efficiency for a 3ω ignition pulse shape, without any advanced conversion schemes, works out to be about 50%, NIF's " $1\ \mu\text{m}$ engine" was designed to produce $\sim 700\text{ TW}$ of 1ω power after $> 3\text{ MJ}$ of $1\ \mu\text{m}$ energy has been extracted. The consequence of this is that NIF's $1\ \mu\text{m}$ laser is necessarily very much larger than the 1.8 MJ specified output. Figure 1 shows current estimates of NIF's maximum performance, plotting the peak 1ω power that the laser can produce as a function of the 1ω energy extracted from the laser. It indicates that NIF's peak, extractable 1ω energy would be $\sim 6.5\text{ MJ}$.

This estimate is for NIF's so-called 11-7 configuration with all seven "slots" in the final

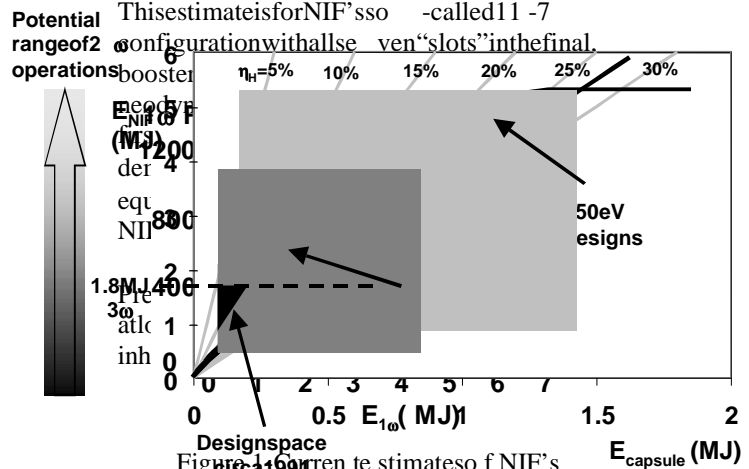


Figure 2-NIF's potential "ignition target design space" with 2ω is very much larger than the design space originally envisioned for NIF.

NIF to drive capsules that absorb ~400 -600 kJ. In this paper we present an assessment of the possibilities offered by operating NIF as a green, 2 ω laser and show how it allows ignition and, even, high yield opportunities far beyond what we originally envisioned when we started NIF in the early 90's. NIF's potential for driving ignition targets with 2 ω can be simply estimated by $E_{\text{cap}} = E_{1\omega} * (\eta_{1-2}) * \eta_H$, where E_{cap} is the capsule absorbed energy, $E_{1\omega}$ is NIF's maximum 1 ω output (~6.5 MJ), η_{1-2} is the conversion efficiency of 1 ω laser energy to 2 ω (~80 -85% average conversion to green are possible) and η_H is the hohlraum coupling efficiency. This gives $E_{\text{cap}} \sim 5 \text{ MJ} * \eta_H$, or capsules absorbing >~1 MJ energy at plausible hohlraum coupling efficiencies of 20 -25% [4].

Figure 2 summarizes a more detailed analysis and graphically shows NIF's potential "ignition target design space" with 2 ω . It plots NIF energy vs. capsule absorbed energy. The light and moderate shaded areas show target design space potentially available with 2 ω at 250 eV peak radiation temperature and 300 eV peak radiation temperature, respectively. We refer to this as target design space because it illustrates all the combinations of NIF energy and capsule energy where an ignition target might be designed at a given peak radiation temperature. Both these design spaces are very much larger than the design space we originally envisioned in ~1991 when we began NIF, shown by the dark triangle in the lower left section.

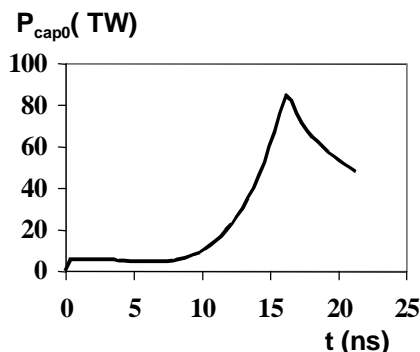


Figure 3-X-ray power absorbed by a 600 kJ, 250 eV graded dopant Be capsule vs. time.

To better appreciate the target design space plots of figure 2 and to understand how they are developed we begin by noting that the light grey, straight lines are lines of constant hohlraum coupling efficiencies, η_H . The bold lines bounding the right hand sides of the 250 eV and

300 eV design spaces are estimates of coupling efficiency for cylindrical NIF ignition hohlraums with a "standard" case: capsule ratio = (hohlraum area/capsule area)^{1/2} of 3.65 [4]. These efficiencies have a slight non-linearity, $\sim (E_{\text{cap}})^{0.1}$. The left hand, vertical boundaries indicate estimated minimum energy of ignition at a given peak radiation temperature. The boundaries drawn combine the approximate minimum energy of ignition at 300 eV, generally taken to be ~100 kJ, and the $T_R^{4.5}$ scaling for minimum energy developed by Lindl, [5] assuming "similar" targets. We note, however, that the minimum energy for ignition can be significantly affected by target design and is the subject of ongoing research. For example Dittrich [6] has designed a capsule which, at 250 eV, also has a minimum energy of ignition of ~100 kJ.

The upper bound of target design space is found

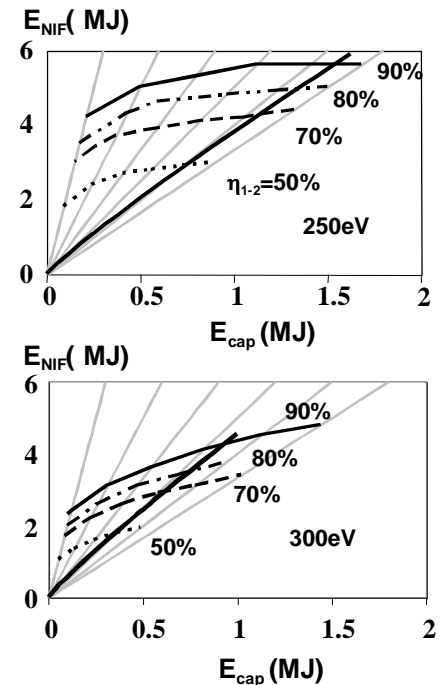


Figure 4-Upper bound on design space for 250 eV (top) and 300 eV (bottom) peak radiation temperatures for 1 ω to 2 ω conversion efficiencies, η_{1-2} , ranging between 50 and 90 %.

ateach hohlraum coupling efficiency by combining target pulse shape requirements with the conversion efficiency, η_{1-2} , of 1 ω to 2 ω light and NIF's 1 ω performance curve, figure 1. The procedure is as follows: Target pulse shape requirements are derived from the x-ray power vs. time absorbed by a given capsule. Figure 3

show the x -ray power absorbed by a 600 kJ, 250 eV graded dopant Be capsule designed by Haan in 1991 (designated “Haan’91”) [4]. We readily scale this capsule’s x -ray power requirements, P_{cap0} , to other absorbed energies via a capsule scaling parameter “ s ”. Multiplying P_{cap0} by s^2 , time by s , and all the dimensions of the capsule by s , scales capsule absorbed energy by s^3 or $E_{\text{cap}} = 600 \text{ kJ} \cdot s^3$ for this scaled capsule. For a given E_{cap} the 2 ω pulse shape requirement is simply $(x\text{-ray power absorbed by the capsule}) / (\text{hohlraum coupling efficiency}) = P_{\text{cap}} / \eta_H$. The 1 ω power produced by the laser must then be $P_{1\omega} = P_{\text{cap}} / (\eta_H \eta_{1-2})$. However, figure 1 provides a constraint on the maximum 1 ω power, requiring $P_{1\omega} = P_{\text{cap}} / (\eta_H \eta_{1-2}) < P_{\text{max}}(E_{1\omega})$ where

$$E_{1\omega} = \int_0^t P_{1\omega} dt. \text{ To find an upper bound at a}$$

given η_H and η_{1-2} we vary the capsule scale size parameter, s , until there is a point in the pulse shape where

$$P_{\text{cap}} / (\eta_H \eta_{1-2}) = P_{\text{max}}(E_{1\omega}).$$

Figure 4 plots these upper bounds for 250 eV and 300 eV peak radiation temperatures for 1 ω to 2 ω conversion efficiencies, η_{1-2} , ranging between 50 and 90%. Note that the upper bounds have a significant dependence on peak radiation temperature and on 1 ω to 2 ω conversion efficiency. The notable difference between the 300 eV and 250 eV upper bounds is because 300 eV capsules require about twice the power of the 250 eV capsules. 300 eV targets are always power limited. It is not unreasonable to think of 250 eV as marking the approximate boundary between designs limited by available power and ones limited by available energy. Analysis at 215 eV, approximately a factor of 2 down in power requirement from 250 eV, shows a design space only slightly larger than the 250 eV space. At 215 eV the targets are mostly limited by the 1 ω energy available (giving a flat upper bound in the $E_{\text{NIF}} E_{\text{CAP}}$ plot), except at the lowest hohlraum coupling efficiencies where they, too, become power limited. We also note that at 300 eV, 50% 1 ω to 2 ω conversion efficiency, the design space is not very much larger than the one we originally envisioned for 300 eV NIF targets.

Figure 2 shows an ignition target design space using 2 ω that is far greater than the target design space that existed in the early ‘90s, when we first started thinking about NIF. At 300 eV the increase comes principally from increased

conversion efficiency, an increase in our expected coupling efficiency [4] and a clearer understanding of how the 1 ω laser will operate. Further expansion of target design space comes from operating at 250 eV rather than 300 eV, where the power requirements as a function of extracted energy are better matched to NIF’s 1 ω capabilities. In order to achieve this performance considerably more green energy must pass through NIF’s final optics assembly (FOA) than the 8 J/cm² of blue light that will pass through the FOA during a 1.8 MJ 3 ω shot. Although this fluence currently defines the state-of-the-art damage limit for 3 ω optics it is expected that approximately a factor of two higher fluences will be possible with green light, compared to blue, without damaging the FOAs. Current thinking is that if full NIF were available today it could reasonably produce between 3 and 4 MJ of green light. With further optics research it is conceivable that 2 ω optics could allow access to the entire design space.

III. Discussion: Benefit of larger design space and 2 ω target physics concerns

The preceding sections showed that NIF, operating at 2 ω , has the potential to greatly increase target design space compared to our original expectations. This increase is desirable for several reasons. First, it allows us to contemplate capsules absorbing far more energy than we originally envisioned. Capsules absorbing ~100 kJ (200 kJ) are on the threshold of failure at 300 eV (250 eV) because of their small size [5, 4]. Basically, as a given ignition capsule is scaled down in size and energy, heat conduction losses play an increasing dominant role in the hotspot power balance, causing 1 ω -D estimates of yield vs. absorbed energy to have a very steep section or “cliff” at low energies. Significantly increasing capsule absorbed energy moves us away from this cliff. Increased capsule absorbed energy is also beneficial because a given capsule’s ability to withstand surface roughness, which seeds hydrodynamic instabilities, increases very dramatically with absorbed energy [7]. Such an important increase in margin, possible with increased capsule absorbed energy, would greatly increase our confidence in achieving ignition and allow us to consider studies of capsule physics and thermonuclear burn physics that are implausible with marginal capsules. A second reason the increase in design space is attractive is that it allows us to consider

a wide range of possible hohlraum sizes and to consider the possibility of trading off capsule absorbed energy for something desirable such as better symmetry or improved diagnostic access.

The increase in target design space potentially available with 2ω makes it appear to be a desirable option for NIF. Unfortunately, virtually all the target physics studies that established the technical basis for NIF ignition [5,8] were done with 3ω light. When we first recognized the possibilities of greenlight nonresonant 2ω database existed. In order to redress this we have been working for several years to answer questions related to using 2ω light on NIF for ignition. This work has been divided into three major areas.

- 1- Laser operations: What performance might we get from NIF at 2ω and how might we actually operate NIF at 2ω . The previous section described the ignition performance we might get with 2ω . Work assessing 2ω operations is ongoing within the NIF project and will be reported elsewhere.
- 2- Projected 2ω ignition target performance assuming Laser-Plasma Interactions are under control. In the next section we describe the results of integrated Lasnex simulations of large 2ω ignition targets.
- 3- Experimental studies of LPI issues for which there is no theoretical predictive capability. The key issues are 2ω propagation, 2ω backscatter and 2ω hot electron production. We have been studying these on both the Helen laser and Omega laser. We summarize current findings in section V.

IV. Lasnex studies of 2ω ignition targets

The target design space potentially available with 2ω light gives us the luxury of being able to consider a wider range of ignition possibilities with Lasnex. Referring to the 250 eV design space of figure 2, we have done integrated Lasnex simulations [9] of two targets that require ~ 3.5 MJ of greenlight. One target, with a standard case: capsule ratio of 3.65, lies on the limiting hohlraum coupling efficiency line, driving a capsule that absorbs ~ 850 kJ of x-rays. A second target demonstrates one of the trade-offs made possible by a very large target design

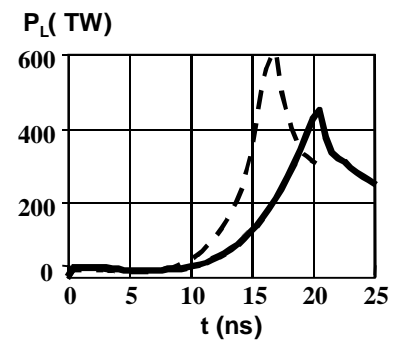


Figure 6- Power pulses required for the 3.65:1 (solid) and 5:1 (broken) case: capsule ratios. Energy under solid (broken) curve is 3.4 MJ (3.3 MJ).

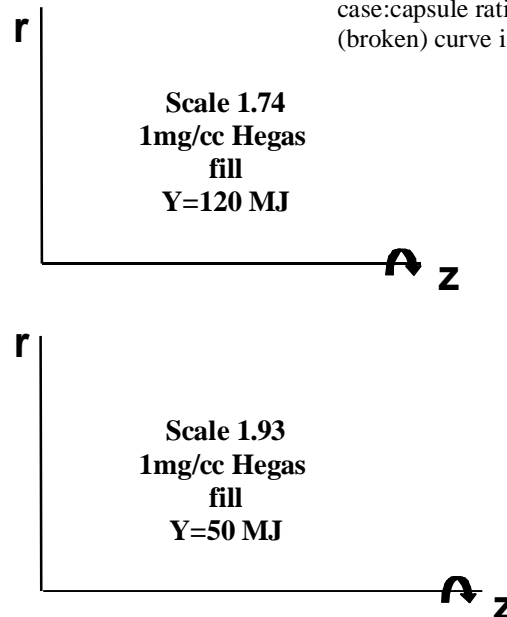


Figure 5- 250 eV 2ω ignition targets modeled with integrated 2D Lasnex simulations. Top: A ~ 1 cm diameter hohlraum with an ~ 4 mm diameter Be capsule absorbing 850 kJ of x-rays. Standard, 3.65 case: capsule ratio. Bottom: A ~ 1.1 cm diameter hohlraum with an ~ 3 mm diameter Be capsule absorbing 400 kJ of x-rays. 5:1 case: capsule ratio. These simulated hohlraums have rotational symmetry around the z-axis and left-right symmetry around the midplane (r-axis).

space. It contains a capsule that absorbs only 400 kJ of x-rays, allowing us to increase the case: capsule ratio to 5.

Figure 5 shows the two targets we simulated with Lasnex. The target with standard, 3.65 case: capsule ratio has a Be "Haan '91" capsule ~ 4 mm outer diameter placed inside a ~ 1 cm diameter cocktail hohlraum [4, 10, 11, 12]. This hohlraum is $\sim 1.74\times$ the size of the NIF point design [13]. The capsule absorbs 850 kJ. In the other target is a scaled version of the same capsule with a diameter of ~ 3 mm. It is inside a cocktail hohlraum ~ 1.1 cm in diameter (scale

1.93), giving a case: capsule ratio of 5.0 and a capsule absorbed energy of ~ 400 kJ. The 2ω pulse shapes we used in simulating the two targets are plotted in figure 6. Both are continuous pulse shapes of approximately 3.5 MJ. The target with larger case: capsule ratio requires higher power because its smaller capsule implodes more quickly; the \sim same amount of energy must come in a short time. As in the original point designs, both targets include a low Z -gas fill (1 mg/cc He) to retard the inward motion of the high Z -hohlraum walls in order to maintain symmetry [13, 14]. We used typical NIF beam pointing as originally developed by Pollaine [13]. A variety of spot sizes were explored in the integrated simulations, including spots as large as ~ 4 mm major diameter by ~ 1.5 mm (3 mm) minor diameter for the 44.5° & 50° (23° & 30°) beam cones. Spots this large are closely matched to the laser entrance hole (LEH) size there by minimizing intensity at the LEH. Integrated simulations with these “big spots”, whose marginal rays come as close to the LEH as $400 - 550 \mu\text{m}$, give results very similar to simulations with considerably smaller spots. Using the large spot size with the 850 kJ capsule’s pulse shape gives a peak single-quad intensity of $\sim 3 \times 10^{14} \text{ W/cm}^2$ ($\sim 1.5 \times 10^{14} \text{ W/cm}^2$) for quadson NIF’s outer (inner) cones.

Extensive, 2D integrated Lasnex simulations indicate 2ω is very promising for ignition. The calculations, using the large spots just described, produce the desired $T_r(t)$ in the hohlraum. Indeed when we perform an identical simulation, except replacing 2ω with 3ω , we find nearly identical $T_r(t)$ profiles. The small differences can be attributed to slightly higher temperature of the hohlraum’s coronal plasma with 2ω . We find that the simulated 2ω beams propagate to the walls and that we can control symmetry in the usual way, by moving the beams and/or adjusting their relative powers [13, 14]. Consequently, we produce adequate symmetry and the capsules ignite and burn in our 2ω integrated simulations. The 850 kJ capsule produces ~ 120 MJ and the 400 kJ capsule produces ~ 50 MJ. Both these yields are close to the 1 Dyiel ds for these particular capsules driven by idealized $T_r(t)$ pulse shapes.

Figure 7 illustrates hot spot shape at ignition time for the two case: capsule ratios. We define ignition time as when the thermonuclear yield rate is set through ~ 2000 TW, a useful rule-of-

thumb criteria. At standard case: capsule ratio we see a hot spot shape that is very familiar from 3 ω design work; a well formed hot spot showing evidence of an incipient jet of cold deuterium-tritium (DT) fuel on the pole together with an incipient curtain of cold DT fuel coming in around the waist of the capsule. Neither perturbation is sufficiently large to affect ignition (indeed, we find at these large absorbed energies that many poorly tuned targets with very much bigger jets and/or curtains will also ignite on the code). At larger case: capsule ratio we see evidence of a trade-off worth further exploration. The symmetry appears to have been improved. This hot spot shows no evidence of a budding pole jet or waist curtain. In tuning the symmetry we find that with these bigger capsules we can achieve adequate symmetry without needing time-dependent “beam phasing”. That is, without continuously and carefully varying the ratio of inner beam power to outer beam power to minimize time-dependent variations in the P2 Legendre component of asymmetry [13, 14]. For a given pointing, one, fixed in time ratio is adequate. That is not to say that with increased coupling energy we still wouldn’t want to try to improve symmetry via some beam phasing. The fact that we don’t necessarily need to use beam phasing in successful integrated simulations is an anecdotal measure of increased robustness due to

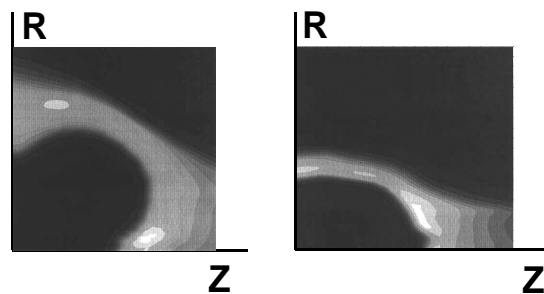


Figure 7—Hot spot shape at ignition time from the integrated simulations. Both produce near 1-Dyiel ds. Left (Right) is the 850 kJ (400 kJ) capsule in a hohlraum of case: capsule ratio 3.65:1 (5:1).

increased absorbed energy.

The weakness of the design simulations just discussed is that neither Lasnex nor any other model can quantitatively predict LPI processes in the complex environment of an ignition hohlraum other than, perhaps, the onset of

filamentation. Increasing the technical basis for NIF we dealt with this shortcoming by doing a wide variety of Nova underdense interaction studies [15, 16, 17, 5, 8] in targets we considered to be "ignition plasma emulators". That is, targets in which we had created, to the degree possible, plasma conditions similar to what we expect in ignition targets. Lasnex integrated simulations of ignition targets defined those plasma conditions. The plasma conditions from our integrated simulations of the 250 eV ignition target at 3.65 case: capsule ratio, at 1 ns after peak power are plotted in figure 8 for the inner and outer cones. According to these plots, LPI for the outer beam principally involves a beam of $\sim 3 \times 10^{14}$ W/cm² interacting with a low-Z plasma with $T_e \sim 4$ keV and electron density ~ 0.1 to $0.14 n_c$, where n_c is the critical density for green light, 4×10^{21} electrons/cm³. For the inner beams, LPI occurs at lower intensity, $\sim 1.5 \times 10^{14}$ W/cm², and in a plasma that changes from He fill-gas to Be ablator blow-off about midway in the beam's path. The plasma density along this path ranges from ~ 0.1 to $0.2 n_c$. These conditions,

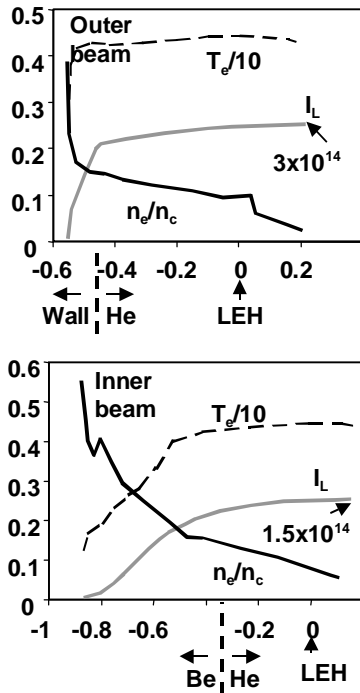


Figure 8- Plasma conditions from integrated simulations of the 3.65 case: capsule ratio target, at 1 ns after peak power. Top for the outer cones, bottom for the inner cones.

then, determine the conditions for empirical studies of laser plasma interactions in a 2ω ignition target and how we might control them.

Ponderomotive filamentation in these conditions can be estimated using a figure of merit.

According to both theory and simulation [18] filamentation of NIF's 8 beams will begin to occur when the filamentation figure of merit (FFOM)

$$I \lambda^2 (n_e/n_c) (3/T_e) > 1 \times 10^{13} \quad (1)$$

and will have a very noticeable effect when the FFOM begins to exceed 2×10^{13} . In this expression I is laser intensity (W/cm²), λ is wavelength (μ m), n_e/n_c is the ratio of electron density to critical density and T_e is electron temperature in keV. For the plasma conditions shown in figure 8, the FFOM at the LEH is 2.5×10^{12} (5×10^{12}) for the inner (outer) beams and peaks at 4×10^{12} (6×10^{12}) 6 mm (5 mm) inside the hohlraum as measured along the beam path from the LEH. These values indicate the 250 eV, 2ω design will be below the threshold for filamentation.

IV. Experimental studies of 2ω Laser Plasma Interaction (LPI)

The key underdense interaction issues for 2ω are essentially the same as they are for 3ω ; propagation, backscatter and hot electron production. For 3ω ignition these issues were studied on the Nova laser during the 1990's as part of the Nova Technical Contract [5, 8] that created the target physics basis for ignition with a NIF class facility. Of these issues, backscatter losses were the greatest concern and were studied in depth while hot electron production, which had never been observed to be large with 3ω , was monitored on Nova but never became the focus of detailed experiments.

In order to establish a database for laser plasma interactions at 2ω we have been studying underdense interactions on the 2ω Helen laser at the Atomic Weapons Establishment (AWE) [19] since 2000 and have converted one beam of the Omega laser at University of Rochester [20] to operate at 2ω [21]. We have been shooting green interaction experiments at Rochester since June, 2002.

The 2ω Omega experiments have principally studied backscatter and are described in greater detail by Moody [22]. Conceptually, the Omega studies are very similar to underdense interaction experiments carried out on Nova to study 3ω .

They use a so-called “gasbag” target comprised of two thin ($\sim 3500 \text{ \AA}$) polyimide membranes glued to either side of an aluminum washer which also has tiny tubes for filling the target with gas. When pressurized, the membranes stretch, forming an oblate spheroid of major diameter $\sim 2.75 \text{ mm}$ and minor diameter $\sim 2.2 \text{ mm}$. These gasbags are heated by 1 ns pulses from 40 of Omega’s beams. The heater beams are defocused to low intensity, nearly filling the bag’s diameter and create a plasma with $T_e \sim 2.5 \text{ keV}$ and scale length $> 1 \text{ mm}$. This plasma is then “probed” by Omega’s single 2ω beam which has $\sim 400 \text{ J}$ in 1 ns pulse. The 2ω probe beam is smoothed by a phase plate which forms a spot that can achieve intensities up to $\sim 1 \times 10^{15} \text{ W/cm}^2$. Backscatter into the $f/6$ lens, the principal quantity studied, is measured by Omega’s Full Aperture Backscatter Station (FABS). At this point, Omega does not yet have a Near Backscatter Imaging diagnostic (NBI) to measure 2ω light scattered just outside the lens. Figure 9 shows one of the scalings we have performed on Omega. It plots 2ω stimulated Raman and stimulated Brillouin reflectivity as a function of intensity from gasbags filled with hydrocarbon gas to a density corresponding to $0.12 n_c$ of green light when the gas is fully ionized. We make several observations from this plot. First, hydrocarbon gas saturates 2ω , like 3ω , mainly produce Raman backscatter at $0.12 n_c$. Second, the peak stimulated Raman backscatter into the lens at intensity approaching 10^{15} is $\sim 15\%$, a typical value for 3ω light at similar conditions. Third, there is a clear intensity scaling to the backscatter that could be interpreted as a threshold for stimulated Raman at low $\sim 10^{14} \text{ W/cm}^2$.

A threshold for Raman backscatter at low $\sim 10^{14} \text{ W/cm}^2$ is encouraging because it can be explained by a filamentation argument and

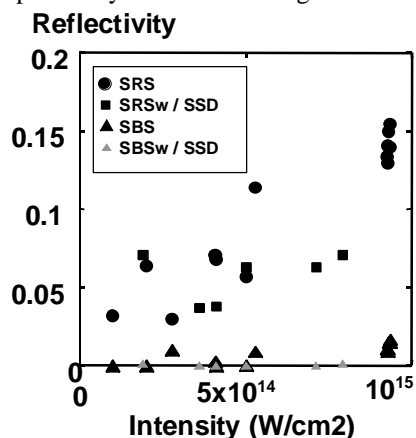


Figure 9-2 2ω Raman and Brillouin reflectivity as a function of intensity. Omega gasbags filled with $0.12 n_c$ of hydrocarbon gas. 250 eV ignition hohlraum can operate at a peak outer (inner) quad intensity of $\sim 3 \times 10^{14}$ (1.5×10^{14}) W/cm^2 .

support for that explanation can be found in the data. At the heart of the filamentation argument is an assumption that Raman backscatter is produced mostly in the hot spot that forms when the beam filaments. That is, if the beam filaments we get Raman backscatter but if the beam doesn’t filament then Raman should be low. In these experiments simple theory and simulations with our laser plasma interaction code F3D [23] indicate a threshold for filamentation around $3 \times 10^{14} \text{ W/cm}^2$. This threshold is supported experimentally by a very narrow Raman backscatter spectrum at 3×10^{14} but very obviously broad Raman backscatter spectra at the higher intensities. (Broad Raman spectra are indicative of filamentation while a narrow spectrum is indicative of little or no filamentation). If the filamentation threshold hypothesis is correct, then this scales favorably to 2ω NIF ignition targets since, according to equation 1, the intensity threshold for filamentation should scale like $\sim T_e$. In Lasnex simulations of 2ω ignition targets $T_e \sim 4.5 \text{ keV}$, vs. $\sim 2.5 \text{ keV}$ in these Omega experiments. Complementing 2ω interaction experiments on Omega have been a wider ranging series of underdense interaction experiments using a single, $\sim 400 \text{ J}$ 1 ns 2ω beam on the Helen laser at AWE. The experiments mostly involved gasbag targets irradiated along the axis of symmetry by a phase-plate smoothed, 2ω spot, typically $\sim 6 \times 10^{14} \text{ W/cm}^2$. A number of small, gas-filled hohlraums were also shot, as well. The experiments are described in detail in a paper by Stevenson [24]. Here we summarize the three most important Helen findings on underdense interaction.

- 1- Propagation: Because the gasbag targets were irradiated by a single beam, we were able to study 2ω propagation via time resolved, side-on x-ray imaging. These side-on images show the formation of well defined plasma columns and closely match synthetic images from simulations with our radiation hydrodynamics code HYDRA [25]. We interpret the good agreement between experimental and synthetic images as evidence that a 2ω beam can propagate in a manner consistent with straight forward hydrodynamics [26] and evidence that, for backscatter production, these targets produced the long scale length plasmas we expected from simulations.
- 2- Effect of composition on backscatter: Helen’s seminal contribution to LPI is the

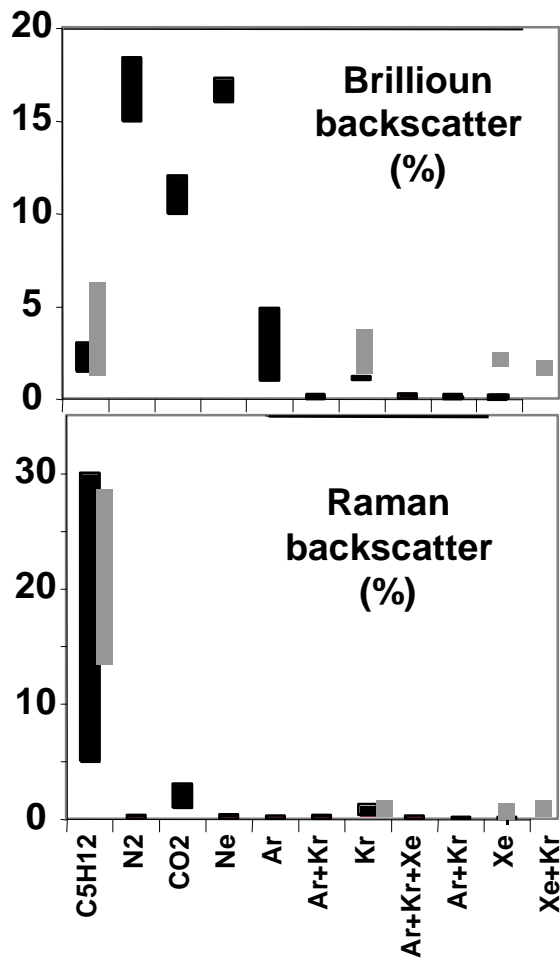


Figure 10-Raman and Brillouin backscatter as a function of composition, ordered in increasing average atomic number, Z . Black bars are Helendata. Grey bars are Omega data.

discovery that plasma composition influences backscatter far more than was previously thought [24]. The black bars on figure 10 show stimulated Raman and Brillouin backscatter from the Helendata gasbag targets as a function of composition, ordered in increasing average atomic number, Z . The vertical extent of a bar indicates the range of backscatter we measured from all targets filled with a given composition. At low Z we see the expected interchange of stimulated Raman for stimulated Brillouin when we switch from a composition with strong ion damping (C_5H_{12}) to a composition with weak ion damping (N_2 , CO_2 , Ne). This is consistent with Nova results [27]. The unexpected finding was the drop in Brillouin with rising Z and the fact that Raman

remained low even as Brillouin dropped. This was inconsistent with a widely held view of an interplay between Raman and Brillouin and that reduction of one results in the increase of the other. These findings have been reproduced in subsequent Omega gasbag experiments using 40 heater beams and one probe. The grey bars in figure 10 plot the Omega results.

- 3- Control of hot electron production: Historically, hot electron production was the bane of early attempts to do ICF with lasers having wavelengths of 1 μm or longer. For example, experiments on the 1 μm Shiva lasers showed hot electron production to rise as hohlraums are driven to higher energy density and that in the highest energy density hohlraums it was possible to convert >20% of the laser energy to hot electrons with a ~50 keV Maxwellian distribution. Such high hot electron fractions prevent ignition by preheating the DT fuel. The discovery in the early '80's that shorter wavelength suppress hot electron production led the community to build subsequent facilities to operate at the shortest wavelength technically feasible, 3 μm . Long experience has justified that decision. Empirically, 3 μm does not efficiently make hot electrons. When considering the possibility of using 2 μm , history cautions to beware of the specter of hot electrons. This is where Helen experiments have made a second original contribution to LPI; hot electron production and how to control it. Measurements of time-integrated, absolute hard x-ray production with Helen's Filter Fluorescer diagnostic (FFLEX) allow us to infer hot electron production. In gasbag targets, we find that C_5H_{12} fills, which efficiently produce Raman backscatter, also produce a rising hot electron fraction as a function of fill density. However, when we switch to other gases, which do not produce much Raman, the hot electron signal remains relatively low, even when the fill density approaches 0.25 n_c. This indicates that plasma composition can control hot electron production, just as it appears to control backscatter. Complementing the gasbag experiments, we also shot small, gas-filled gold hohlraums on Helen in order to further study hot electron production. These experiments used unsmoothed beams, with

best focus ($\sim 80 \mu\text{m}$ diameter) at the LEH. Figure 11 plots hot electron fraction observed with these hohlraums as a function of fill density, for two fills, C_5H_{12} and Kr. With C_5H_{12} there is a striking increase in hot electron production with fill density with a peak, inferred hot electron fraction of $\sim 20\%$ in the vicinity of $0.25n_c$. However, when we change the fill gas to Kr, we find relatively little hot electron production, even near $0.25n_c$. Backscatter measurements on these hohlraums also show that Raman is relatively high in the C_5H_{12} hohlraums but very much reduced in the Kr filled hohlraums. These Hellen experiments suggest two rules-of-thumb for designing 2W ignition targets with low hot electron production. Keep most of the LPI volume below $0.15n_c$ and/or judiciously choose materials to avoid Raman producers.

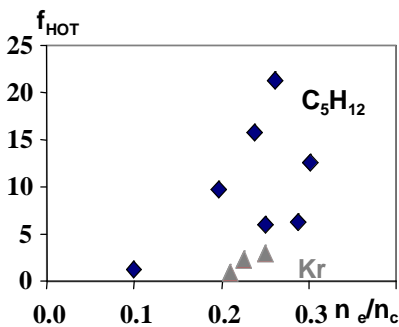


Figure 11- Hot electron fraction in small, gas filled Hellen hohlraums as a function of fill density. C_5H_{12} , black spots, and Kr, grey triangles.

V. Alternative ignition hohlraum designs

The finding that we can control backscatter and hot electron production via judicious choice of plasma composition is potentially very important for NIF because it implies that we can control LPI at target design. This has engendered a new area of target design, exploring targets where the conventional He/Hgas-filled ignition point [13, 14] is replaced by other materials. A constraint on these designs is a preshot temperature of $\sim 18^\circ\text{K}$ needed for the cryogenic capsule. This eliminates most gases since they would freeze out.

Our exploration of alternative hohlraum designs has been exclusively on variants of the standard case: capsule radiating target of figure 5, using the

pulse shapes shown by the solid line of figure 6 and the 850 kJ Be capsule. Our investigations fall into two cryogenic-compatible classes; designs where the He gas fill is replaced by a foam and designs where it is largely replaced by an inert Zor high-Z liner. In the foam designs we replaced the 1 mg/cc He gas by 1 mg/cc SiO_2 (this foam exists) or 1 mg/cc GeO_2 and, even, 1 mg/cc XeO_2 (this foam cannot exist but allows us to study the scaling with Z). The lined targets we studied included hohlraums lined with 1 μm solid (frozen) Kr and 1 μm frozen Xe.

The result of these integrated simulations is that it appears possible to replace the He or He-Hgas in NIF hohlraums with mid to high Z material and still maintain drive and symmetry adequate for ignition. The calculated $T_R(t)$ from hohlraum simulations using the three different foams are close to what is calculated for He fill. The simulated hot spot shapes at ignition do not look very much different than the one found with He fill, in figure 7. The capsules work in these integrated simulations, producing yields $\sim 120\text{MJ}$, similar to He filled targets. It was not necessary to make any design changes compensating for the increased x-ray preheat of the higher-Z foams. The principal drawback is that the hohlraum has a greater propensity to produce a pole high implosion as we raise the average Z of the fill. In this study we counteracted this tendency by switching a greater fraction of the laser power to the inner beams. If the pole-high tendency cannot be offset by some other change, such as geometry, this might limit the upper bound to the Z of the foam.

In addition to the foam simulations, we also investigated replacing the He gas with 1 μm liners of either Kr or Xe. Although these designs readily produced the required $T_R(t)$, we were unable to find a symmetry solution for vacuum hohlraums with liners. Axial stagnation of the liner material at late times generated a pole-high x-ray pulse that could not be offset by raising the power of the inner beams. However, if we included a very low fill of He, 0.1 mg/cc, we found we could tune the symmetry. In these simulations we again found it necessary to raise the fraction of power to the inner beam in order to tune the symmetry.

All these simulations of alternative hohlraums predict coronal electron temperatures considerably higher than the $\sim 4.5\text{keV}$ temperature in the He filled design, shown in

figure 8. For example, the targets filled with SiO_2 have $T_e \sim 7 \text{ keV}$. High temperature reduces the filamentation figure of merit, equation 1, and, in principle, makes such hohlraums less likely to suffer from filamentation. However, increased resistance to filamentation allows one to contemplate higher laser intensity and, therefore, higher radiation temperature designs. Thus, hohlraums with compositions other than the conventional He or He-H in the beam path may be a pathway to higher radiation temperatures with 2ω .

These few preliminary simulations of alternative hohlraums are far from being detailed point designs. However, they do show that it is possible to consider replacing the He or He-H gas of the conventional NIF designs with some other material and still be able to produce the required drive and adequate symmetry for ignition. This, in turn, means that it could be possible to engineer LPI in 2ω (or, even, 3ω) ignition designs by engineering the plasma composition in the beam paths. Alternative hohlraums are a new area of investigation that we will be examining in the coming years.

Acknowledgements

This work performed under the auspices of the U.S. Department of Energy by the Lawrence Livermore National Laboratory under Contract No. W-7405-Eng-48.

References:

- 1- J.A. Paisner, E.M. Campbell and W.J. Hogan, *Fusion Technol.* **26**, 755 (1994)
- 2- R.S. Craxton, "Theory of high efficiency third harmonic generation of high power Nd-glass radiation." *Opt. Commun.* **34**, 474-478 (1980); B.M. Van Wonterghem et al., *Appl. Opt.* **36**, 4932 (1997).
- 3- K. Manes, M. Spaeth, LLNL, private communication, 2003.
- 4- L. Suter, J. Rothenberg, D. Munro, B. Van Wonterghem and S. Haan, *Phys. Plasmas* **7**, 2092 (2000).
- 5- J.D. Lindl, *Phys. Plasmas* **2**, 3933 (1995).
- 6- T. Dittrich, S.W. Haan, M.M. Marinak, S. Pollaine, and R. McEachern, *Phys. Plasmas* **5**, 3708 (1998).
- 7- S.W. Haan, T. Dittrich, G. Strobel, S. Hatchett, D. Hinkel, M. Marinak, D. Munro, O. Jones, S. Pollaine, and L. Suter, "Update on ignition target fabrication specifications," *Fusion Science and Tech.* **41**, 165 (2002); G. Strobel, S.W. Haan, et al. Submitted for publication.
- 8- See National Technical Information Service Document No. DE96010473, 1996 ("Special Issue: *Nova Technical Contract*" ICF Quarterly Report, July-September 1995, p. 209 (UCRL-LR-105821-95-4)). Copies may be ordered from the National Technical Information Service, Springfield, VA 22161.
- 9- L.J. Suter, A.A. Hauer, L.V. Powers, et al., *Phys. Rev. Lett.* **73**, 2328 (1994).
- 10- T.J. Orzechowski, M.D. Rosen, H.N. Kornblum, et al., *Phys. Rev. Lett.* **77**, 3545 (1996).
- 11- D. Colombant, M. Klapisch and A. Bar-Shalom, *Phys. Rev. E* **57**, 3411 (1998).
- 12- H. Nishimura, T. Endo, H. Shiraga, Y. Kato and S. Nakai, *Appl. Phys. Lett.* **62**, 1344 (1993).
- 13- S.W. Haan, S.M. Pollaine, J.D. Lindl et al., *Phys. Plasmas* **2**, 2480 (1995).
- 14- W.J. Krauser, N.M. Hoffman, D.C. Wilson, et al., *Phys. Plasmas* **3**, 2084 (1996).
- 15- B.J. MacGowan, B.B. Afeyan, C.A. Back, R.L. Berger, *Phys. Plasmas* **3**, 2029 (1996).
- 16- S.H. Glenzer, L.J. Suter, R.E. Turner et al., *Phys. Rev. Lett.* **80**, 2845-2848 (1998).
- 17- J.D. Moody, B.J. MacGowan, J.E. Rothenberg, et al., *Rev. Lett.* **86**, 2810-2813 (2001).
- 18- E.A. Williams, LLNL, private communication (1999).
- 19- M.J. Norman, J.E. Andrew, T.H. Bett et al., *Appl. Opt.* **41**, 3497 (2002).
- 20- J.M. Soures, R.L. McCrory, C.P. Verdon et al., *Phys. Plasmas* **3**, 3108 (1996).
- 21- A. MacKinnon, *Rev. Sci. Instr.*, submitted for publication (2003).
- 22- J. Moody, et al., Proceedings of the Third International Conference of Inertial Fusion Sciences and Applications, Monterey, CA, 2003 (to be published).
- 23- C.H. Still, R.L. Berger, A.B. Langdon, et al., *Phys. Plasmas* **7**, 2023 (2000).
- 24- M. Stevenson, *Phys. Plasmas*, 2004 (to be published).
- 25- M.M. Marinak, G.D. Kerbel, N.A. Gentile, et al., *Phys. Plasmas* **8**, 2275 (2001).
- 26- N. Mezzan, et al., Proceedings of the Third International Conference of Inertial Fusion

Sciences and Applications, Monterey, CA,
2003 (to be published).

- 27- D.S. Montgomery, B.B. Afeyan, J.A. Cobble
etal, Phys. Of Plasmas, . **5**, 1973 (1998)